



# SSR1 Tuner studies

*(work in progress)*

L. Ristori

*With slides from I. Gonin, M. Hassan and D. Passarelli*



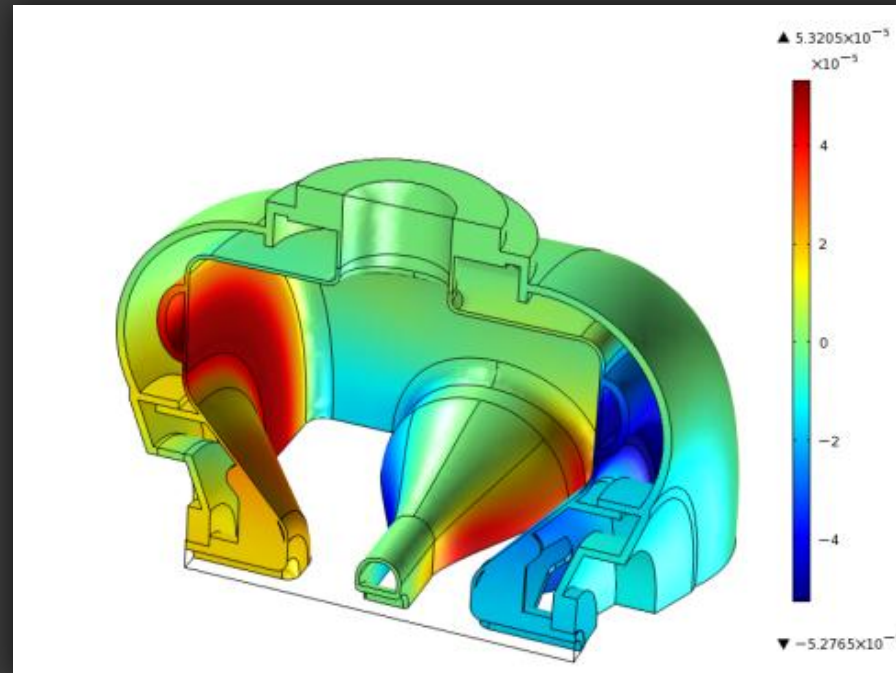
# Overview

- ⦿ Reduce the sensitivity to He pressure fluctuations of the system cavity+vessel+tuner.
- ⦿ Allow access for maintenance to motor and piezos through access port
  - move piezos away from beam pipe
- ⦿ Guarantee an acceptable tuning efficiency (stroke of beam pipe / stroke of motor+piezos, >50%).
  - High rigidity of tuner and/or low rigidity of cavity
  - Mechanical advantage as close to 1:1 as possible (we had 1:5 in the prototype)
- ⦿ Guarantee an acceptable tuning Range (+/- 200 kHz)
  - Avoid yield
  - Limit the forces required



- **Cavity + vessel** design was developed for  $df/dP \approx 0$
- The movable beam pipe (left in picture) was left free (conservative approach).

- Comsol multiphysics  
 $df/dp \sim 4.9$  Hz/Torr
- Ansys multiphysics  
 $df/dp \sim -1$  Hz/Torr
- Ansys mechanical  
 $df/dp \sim 2.6$  Hz/Torr



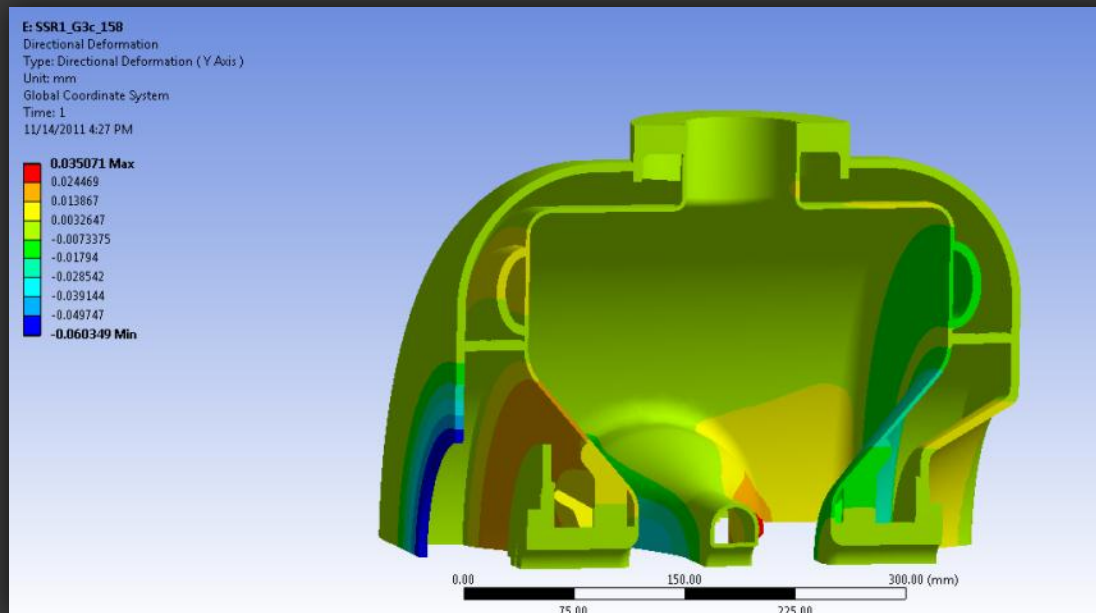
- A **Ring** couples the cavity end walls with the helium vessel end walls.



- The Diameter of the Ring has influence on several aspects.
- Of major importance is the **robustness of the  $df/dP$**  value, how stable it is for small variations of the actual cavity+vessel shape.
- We can predict (Passarelli) the  $df/dP$  value by looking at the deformations of the helium vessel at the connection points with the cavity (here called  $d_{Ring}$  and  $d_{BP}$ ).
- Ring  $D=125$  mm,  $df/dP = -0.20 d_{Ring} - 0.53 d_{BP} + 23$  (Hz/torr)
- Ring  $D=140$  mm,  $df/dP = -0.18 d_{Ring} - 0.52 d_{BP} + 21$  (Hz/torr)
- **Ring  $D=158$  mm,  $df/dP = -0.01 d_{Ring} - 0.29 d_{BP} + 8.5$  (Hz/torr)**
- Lower coefficients for deformations at the Ring and Beam Pipe give a more stable  $df/dP$
- A **larger Ring Diameter is favorable** in this case



- Study with Ring D = 158 mm
- $Df/dP = 5 \text{ Hz/torr}$  (free BPs),  $7 \text{ Hz/torr}$  (fixed BPs)
  - And  $df/dP = -0.01 \text{ dRing} - 0.29 \text{ dBP} + 8.5 \text{ (Hz/torr)}$
- A Larger ring also reduces the stiffness of the cavity to tuning.

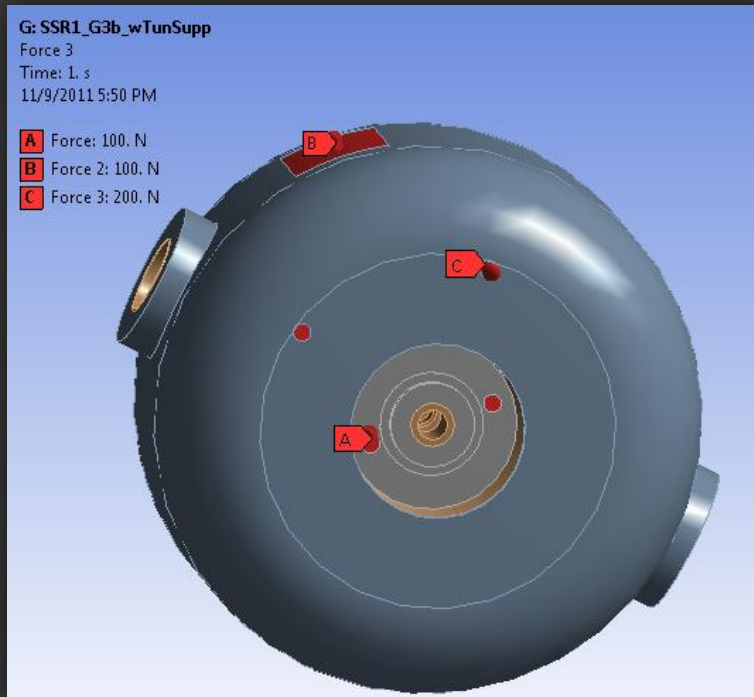


Deformations induced on the cavity+vessel with ring D=158 mm, due to 1 atm He pressure.

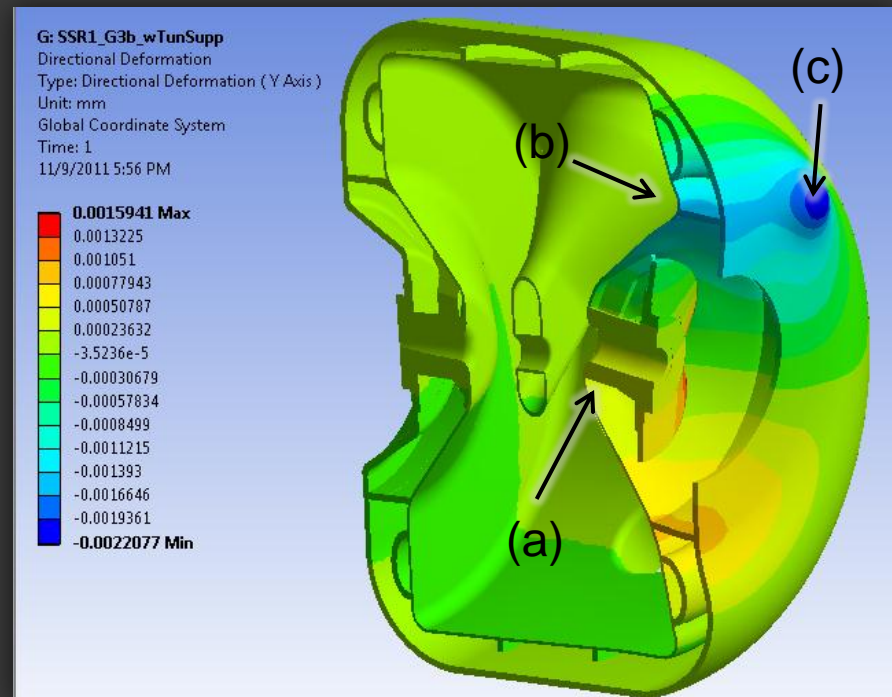
Beam pipes deformations in the order of few  $\mu\text{m}$ .



- If we introduce a tuner similar to the **lever prototype**, the cavity deforms in an unwanted way.
- The **G3 vessel is more flexible** than the prototype



Interface areas:  
A: tuning forces on cavity  
B: motor reaction forces  
C: pivoting point reaction forces

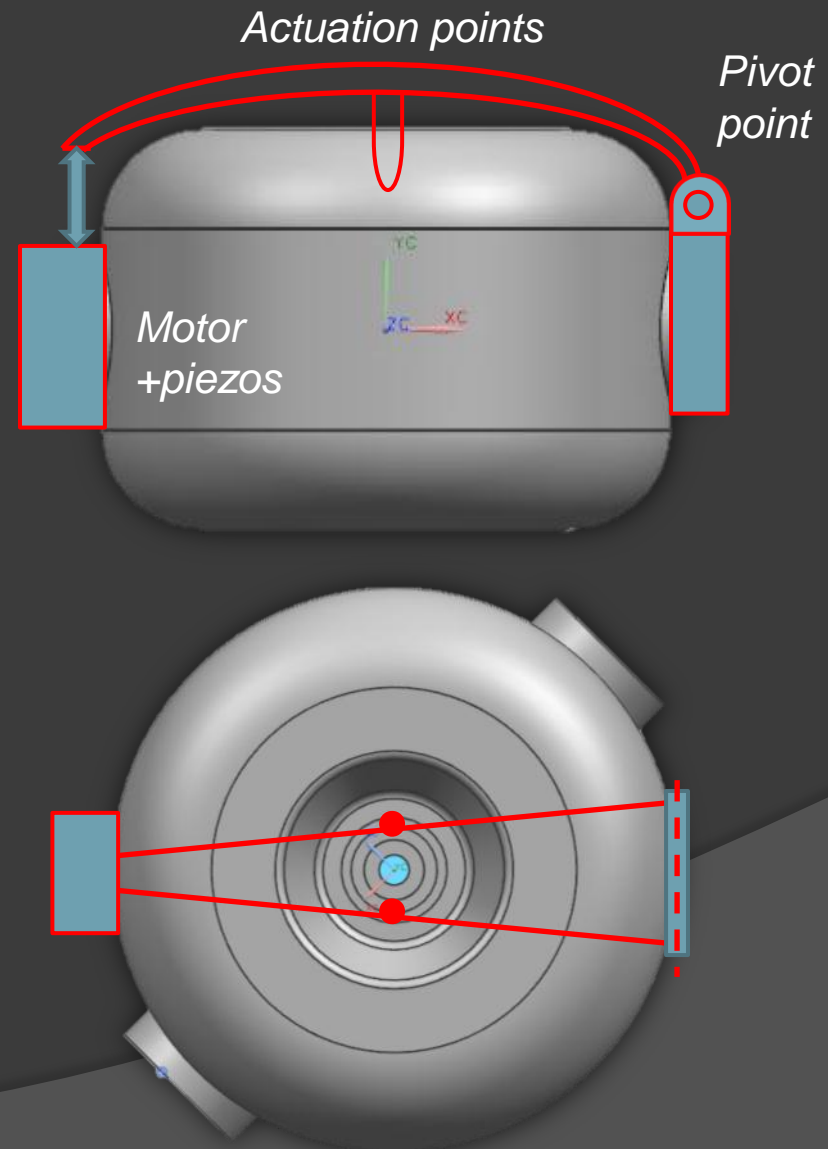
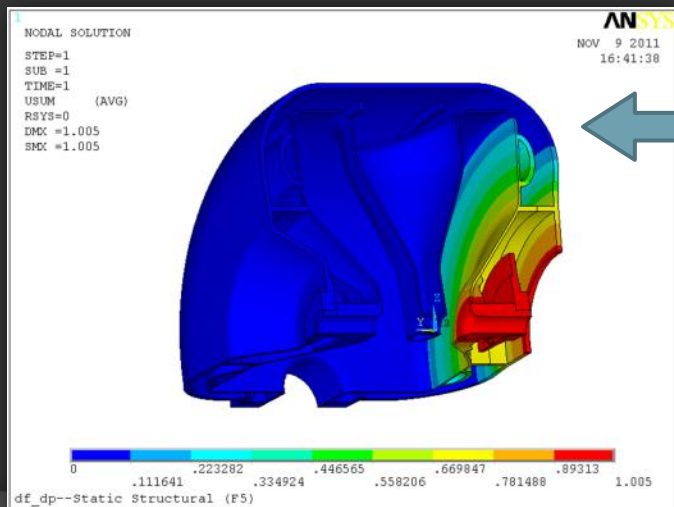


When subject to an arbitrary tuning force, the beam pipe area appears to rotate (a) more than translate.  
Also, the end-wall shape is distorted (b) due to the reactions on the vessel wall (c)



◉ If we change the leverage layout for the tuner:

- Translation of Beam Pipe
- Mechanical advantage reduced to 1:2 (lower is better for piezo stroke requirements)
- Reduced stiffness of cavity (increased tuning efficiency)
  - Vessel wall and cavity wall move in the same direction, the reaction forces do not “fight” the tuning forces





## Ahead:

- ◎ **Optimal diameter for the Ring**, can we place it on top of the donut rib (how large can it be) before we see the  $df/dP$  diverging to negative values?
  - Easier welding
  - Lower stiffness to tuning
- ◎ Tuning forces on cavity+vessel, do they **alter the  $df/dP$** ?
  - If yes, can we minimize this effect by design?
- ◎ Tuner design
  - Identify the optimal **interface locations**
  - Evaluate the required stiffness of the lever arm to guarantee an acceptable **tuning efficiency** (beam pipe stroke/ motor+piezo stroke )